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THERMTRAJ: A Fortran Program to Compute the Trajectory and Gas Film Temperatures of Zero Pressure Balloons

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February 1983





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Prepared Under Contract No. NAS6-3072



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THERMTRAJ: A FORTRAN PROGRAM TO COMPUTE THE TRAJECTORY AND GAS AND FILM TEMPERATURES OF ZERO PRESSURE BALLOONS

Ву

Walter J. Horn and Leland A. Carlson Texas A&M University

SUMMARY

A FORTRAN computer program called THERMTRAJ is presented which can be used to compute the trajectory of high altitude scientific zero pressure balloons from launch through all subsequent phases of the balloon flight. In addition, balloon gas and film temperatures can be computed at every point of the flight. The program has the ability to account for ballasting, changes in cloud cover, variable atmospheric temperature profiles, and both unconditional valving and scheduled valving of the balloon gas. The program has been verified for an extensive range of balloon sizes (from 0.5-41.47 million cubic feet). Instructions on program usage, listing of the program source deck, input data deck and printed and plotted output for a verification case are included.

INTRODUCTION

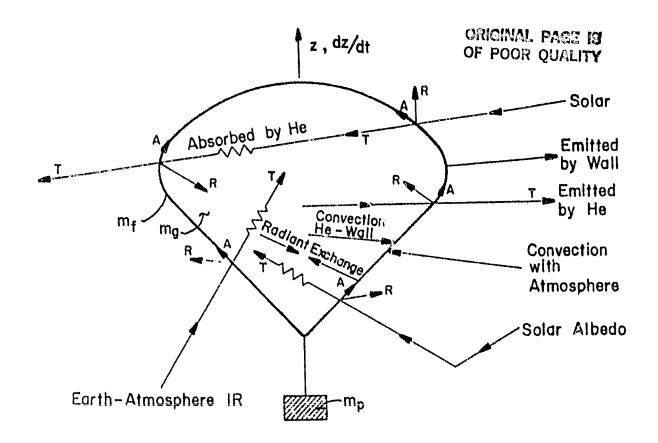
The program described in this report was developed under NASA Contract NAS6-3072 to accurately compute the trajectory of high altitude scientific zero pressure balloons, and to compute the balloon film and gas temperature. A set of five ordinary differential equations based

upon the dynamics and thermodynamics of the balloon system have been formulated. These equations are solved using a fourth order Runge-Kutta solution scheme with a variable time step. The program allows the user to specify a ballast schedule, to select from five atmospheric models (or supply his own) to adjust for changes in cloud cover and to account for balloon gas valving.

The background analysis for the computer program is contained in the reference, "A Unified Thermal and Trajectory Model for the Prediction of High Altitude Balloon Performance." The purpose of this report is to detail the use of the computer program. The following section is a presentation of the governing ordinary differential equations and the details of the options available to the user of the program. Subsequent sections will deal with the input data requirements and formats, the output format (both printed and plotted), a program listing, and the results of a verification study conducted during the development of the program.

PROBLEM DESCRIPTION

The trajectory of a balloon system is dependent upon the dynamics of the system and the thermal contributions from its atmospheric environment. Figure 1 contains a schematic of a typical zero-pressure balloon system indicating the source of thermal loading on the system. The results of the analyses are reported in the Reference. They show that the vertical motion of the balloon is governed by the following set of five ordinary differential equations:



Symbols: T = Energy transmitted

R = Energy reflected

A = Energy absorbed

 m_p = Mass of payload plus ballast

 m_f = Mass of balloon film

 m_q = Mass of balloon gas

Figure 1. Schematic of typical balloon system with the thermal inputs to the balloon.

$$\frac{dv}{dt} = \frac{g(\rho_a V_g - m_f - m_g - m_p) - (\rho_a C_D v^2 \overline{A})/2}{m_g + m_f + m_p + 1/2 \rho_a V_g}$$
(1)

$$\frac{dz}{dt} = v$$

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(2)

$$\frac{dm_g}{dt} = \frac{p_g M_g}{RT_g} \dot{e}_g - \dot{e}_V$$
 (3)

$$\frac{dT_f}{dt} = \frac{Q_f}{C_f m_f} \tag{4}$$

$$\frac{dT_g}{dt} = c \frac{1}{p_g m_g} \qquad \left[Q_G - \frac{g M_a m_g T_g v}{T_a M_g} \right]$$
 (5)

where: t = time

v = vertical velocity of the balloon system

g = acceleration due to gravity

 ρ_a = density of air

 $V_{\rm q}$ = volume of the balloon

 m_f = mass of the balloon film

 $m_q = mass of gas$

 m_p = mass of the payload = mass of the balloon system - $(m_f + m_q)$

 C_D = coefficient of drag

 \overline{A} = effective balloon cross-sectional area = 1.2089 $V_g^{2/3}$

z = balloon altitude

p_q = balloon gas pressure

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 ${\rm M_{
m g}}$ = molecular weight of balloon gas

R = universal gas constant

 T_q = temperature of the balloon gas

 $\dot{\mathbf{e}}_{\mathbf{g}}$ = volume flow rate of gas exhausted at entry into float

 $\dot{\mathbf{e}}_{_{\mathbf{V}}}$ = mass flow rate of balloon gas during controlled valving operation

 T_f = temperature of balloon film

 Q_f = net heat flux to film

 C_f = specific heat of balloon film

 C_{p_g} = specific heat of balloon gas

 Q_{G} = net heat flux to balloon gas

 M_a = molecular weight of air

 T_a = temperature of the air

and the radiative heat transfer to the balloon film can be expressed as

$$Q_{F} = \frac{1}{4} G \alpha_{W, eff} + \frac{1}{2} G r_{e} \alpha_{W, eff} + \epsilon_{int} \sigma (T_{g}^{4} - T_{f}^{4}) + CH_{gf} (T_{g} - T_{f}) + CH_{fa} (T_{a} - T_{f}) - \epsilon_{W, eff} \sigma (T_{f}^{''} - T_{BB}^{4})$$
 (6)

while the radiative heat transfer to the balloon gas can be expressed as

$$Q_{G} = G_{\alpha g,eff} (1+r_{e}) - \epsilon_{int} \sigma (T_{g}^{\mu} - T_{f}^{\mu}) - CH_{gf} (T_{g} - T_{f})$$

$$- \epsilon_{g,eff} \sigma T^{\mu} + \epsilon_{g,eff} \sigma T_{BB} S$$
(7)

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Where the effective coefficient of absorptivity of the balloon film, the effective coefficient of infrared interchange between the balloon film and gas, the effective coefficient of emissivity of the balloon film, the effective coefficient of absorptivity of the balloon gas, and the effective coefficient of emissivity of the balloon gas are expressed in terms of the gas and film radiative properties as:

$$\alpha_{\text{w,eff}} = \alpha_{\text{w}} \left[1 + \frac{\tau_{\text{w,sol}} (1 - \alpha_{\text{g}})}{1 - r_{\text{w,sol}} (1 - \alpha_{\text{g}})} \right]$$
 (8)

$$\varepsilon_{\text{int}} = \frac{\varepsilon_{\text{g}} \varepsilon_{\text{W}}}{1 - r_{\text{w}} (1 - \varepsilon_{\text{g}})}$$
 (9)

$$\varepsilon_{\text{w,eff}} = \varepsilon_{\text{W}} \left[1 + \frac{\tau_{\text{W}} (1 - \varepsilon_{\text{g}})}{1 - r_{\text{W}} (1 - \varepsilon_{\text{g}})} \right]$$
 (10)

$$\alpha_{g,eff} = \frac{\alpha_g \quad \tau_{w,sol}}{1 - r_{w,sol} \quad (1-\alpha_g)}$$
 (11)

$$\varepsilon_{g,eff} = \frac{\varepsilon_g \tau_W}{1 - r_W (1 - \varepsilon_g)}$$
(12)

where G = solar constant

 r_{α} = earth reflectivity (albedo)

σ = Stefan-Boltzman constant

 $\mathrm{CH}_{\mathrm{gf}}^{\mathrm{=}}$ convective heat transfer coefficient between the balloon film and gas

CH_{fa} = convective heat transfer coefficient between the balloon film and air

 T_{RR} = black ball temperature

S = balloon surface area = $4.835976 \text{ V}_g^{2/3}$

 $\alpha_{_{\mbox{\scriptsize W}}}$ = coefficient of absorptivity of the balloon film in the infrared spectrum

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- τw,sol = coefficient of transmissivity of the balloon film in the solar spectrum
 - $\boldsymbol{\alpha}_{\boldsymbol{\sigma}}\text{=}$ coefficient of absorptivity of the balloon gas
- $r_{w,sol} = {coefficient \ of \ reflectivity \ of \ the \ balloon \ film \ in \ the \ solar \ spectrum}$
 - $\epsilon_{\sigma}^{=}$ coefficient of emissivity of the balloon gas
 - $\boldsymbol{\varepsilon}_{_{\!\boldsymbol{W}}}^{}\text{=}$ coefficient of emissivity of the balloon film
 - $r_{w}^{=}$ coefficient of reflectivity of the balloon film in the infrared spectrum
 - $\tau_{\rm W}^{=}$ coefficient of transmissivity of the balloon film in the infrared spectrum

Differential equations 1 through 5, along with the defining equations 6 through 12, are solved using a Kutta-Simpson, one-third rule, fourth order Runge-Kutta solution technique.

The atmospheric properties are computed using any of five "standard" atmosphere models or a user supplied model. The five standard models are the 1962 Standard Atmosphere model and four models based upon NSBF temperature-altitude profiles measured during the winter, spring, summer and fall of the year.

Ballasting is accomplished by providing a ballast rate-time schedule corresponding to the actual ballast schedule of the balloon flight being simulated. This schedule represents the ballasting rate at all times during the flight; therefore, each ballasting operation is represented with an entry at both the beginning and the end of the ballast drop.

Controlled balloon gas valving operations are modelled in a manner similar to that for ballast drops. That is, a valving mass flow rate-time schedule is provided for every point of the flight. Therefore, every valving operation is represented by two entries in the valving schedule; one

at the beginning of the valving operation and one at the end. Valving of the balloon gas at the entry into float is handled automatically by the program by monitoring the volume of the balloon. When the balloon volume exceeds the maximum volume of the balloon during a time step in the solution, a sufficient volume of gas is expelled to prevent the volume of the balloon from exceeding the maximum volume of the balloon and a smaller time step is used in the solution.

Cloud cover conditions are specified by a time schedule of albedo values and black-ball temperature profile adjustments at every point in the flight. Therefore, if accurate cloud cover information is available for the balloon flight being simulated it can be modelled within the program.

A variable time step solution of the governing differential equations was developed to economize the solution scheme. Basically, the procedure followed was to double the time step if the computed values of the increment of the balloon altitude, velocity, and film temperature and gas temperature were less than some user provided tolerance for the previous three steps in the solution. In a similar manner, the time step was reduced by a factor of 0.5 if the computed values of the same increments mentioned above exceed the user provided tolerance during any step of the solution and that solution step was repeated.

PROGRAM USAGE

The computer program is written in FORTRAN IV programming language and is operational on the Texas A&M Amdahl 470 V/6 and Amdahl 470 V/7B computers.

The program uses plotting subroutines developed by California Computer Products, Inc. (Cal-Comp) which are available on the Texas A&M computer system.

This section gives an outline of the procedure for using the THERMTRAJ program for solving the equations, developed in Reference 1 and summarized in the previous section of this report, governing the vertical motion of the balloon system. Table 1 contains a summary of the input data cards necessary to run a flight simulation and Table 2 contains a summary of the units of the input data. Table 3 contains a list of the default values of the input variables for the program. Only those variables that are to be modified need to be assigned values on the data card associated with the READ (5, FIPUT) statement of line 91 of the source program listing of Appendix A. Table 4 contains a list of the FORTRAN variable names used in the program and their definitions. Table 5 contains a summary of the output of the program.

Figure 2 contains a typical four segment atmospheric temperaturealtitude profile used to define the atmospheric properties at each point in the balloon flight and Figure 3 contains a summary plot of the five optional profiles that are contained in the THERMTRAJ program. A typical three segment black-ball temperature-altitude profile is presented in Figure 4 indicating the FORTRAN symbolic names of the coordinates of each of the break-points on the profile.

The user may begin the balloon simulation at any point of the balloon flight. The following input data in the NAMELIST FIPUT must be modified to correspond to the conditions which exist at the point the simulation is initialized:

TIMOL - Time of initialization of simulation (hrs)

CUTDT - Length of flight from the point the simulation was initiated (hrs)

ASCRT and HFLIT - Must be adjusted so that

HFLIT - BALT ASCRT

yields either the time from initial start to the estimated time of float <u>or</u> the time when TBBC(I) is to be used instead of the three segment TBB profile

MGAS - Mass of gas at the start of the simulation (g)

MPAYI- Mass of payload, including <u>remaining</u> ballast at the start of the simulation (g)

All other NAMELIST variables are as if the computations were started at the original launch time and altitude.

The variables of the ballast drop schedule, the cloud cover schedule and the valving schedule must also be modified to correspond to the initial start time of the simulation. Specifically, the times in the arrays TBDRP(I), TCLDC(I), and TVALVE(I) must be times measured from the time of the initialization of the flight simulation, not from the launch time of the balloon.

All input experimental data (EMB, EAIRT, EFILMT, EGAST) must be for times which occur after the time of the start of the simulation.

Finally, the value of four variables within the body of the main program must be altered to correspond to the actual beginning of the simulation. The initial values of TR, TS, Z1, and Z2 (see lines 281-284 of the source deck of Appendix A) must be balloon gas temperature, film temperature, altitude, and velocity at the time of the beginning of the simulation.

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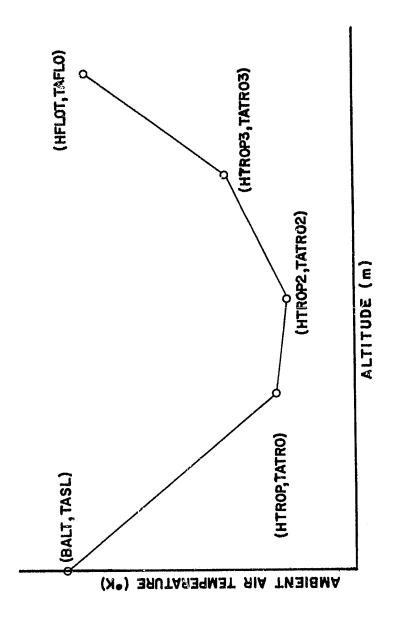
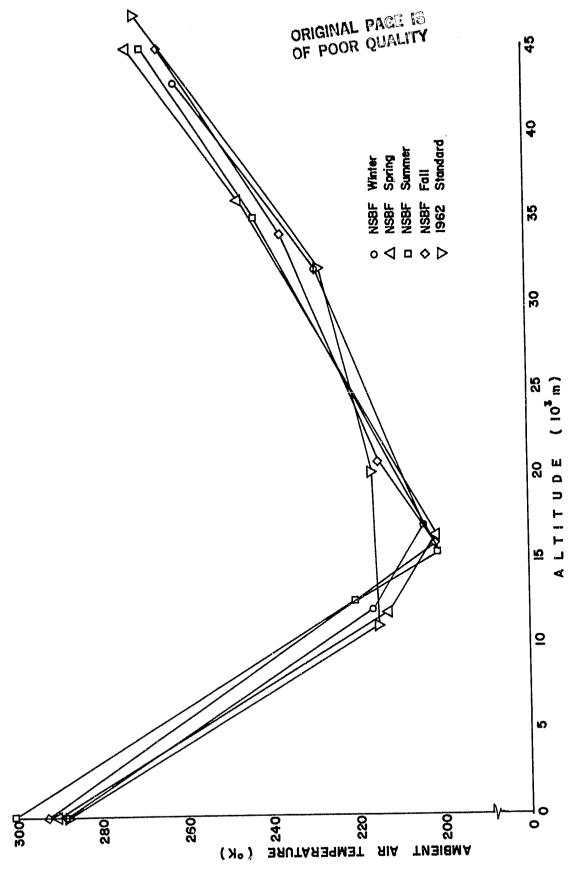


Figure 2. Typical Atmospheric Temperature Model



Five optional atmospheric temperature profiles available in the THERMTRAJ program Figure 3.

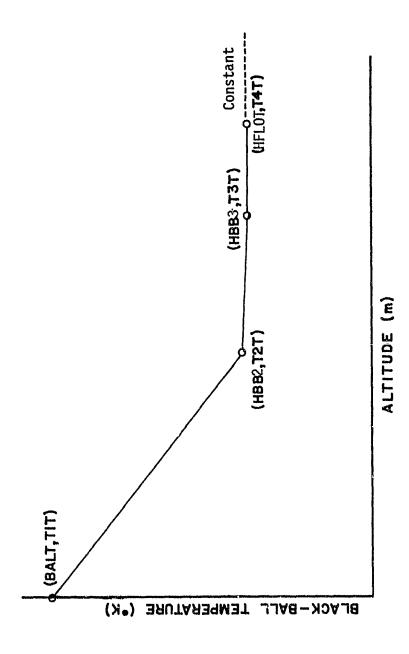


Figure 4. Typicaï black-ball temperature profile

Table 1. Summary of Input Cards

Read Order	Variables	Format.
1	NTITLE	20A4
2	NAMELIST/FIPUT/TIMOL, CUTDT, BALT, ASCRT, HFLIT,	Namelist
•	PASL, MASSF, MGAS, MPAYI, VOLMAX, DAYL, TWILT, ALBED,	
	FLSOD, PTINC, DTMAX, SPHTW, SPHTG, MOLA, MOLG, ALFRES,	
	EG,ALFSO,TWSOL,RWSOL,EW,RW,TAUW,TASL,HTROP,TATRO	
	HTROP2, TATRO2, HTROP3, TATRO3, HFLOT, TAFLO, HBB2, HBB3,	
	T2T,T3T,T4T,DPLT,IATMS	
3	NBDRP	
4	TBDRP(I) and BRATE(I); I=1,NBDRP	2F10.2
	(omitted if NBDRP=0)	
5	NCLDC	15
6	<pre>TCLDC(I),ALBC(I) and TBBC(I)</pre>	3F10.2
	(omitted if NCLDC=0)	
7	NVALVE	
8	TVALVE(I) and VALVRT(I)	2F10.2
	(omitted if NVALVE=0)	
9	NEX	13
10	ELN1, ELN2, ELN3	3F3.0
	(omitted if NEX=0)	
11	TT(J),J=1,3; EMB(I),EAIRT(I),EFILMT(I),EGAST(I)	3F3.0,1X,
	(omitted if NEX=0)	4F10.4

Table 2 Summary of Units of Imput Data

TIMOL - CUTDT - BALT - ASCRT - HFLIT -	hrs. hrs. m m/min. m	ORIGINAL OF POOR	HTROP3 TATROP3 HFLOT TAFLO HBB2	on. bes on NA	m °K [©] K
PASL - MASSF -	millibars g		HBB3 T2T		o.K
MGAS - MPAYI -	g g		T3T T4T	**	°K °K
VOLMAX - DAYL -	g m3 hrs.		DPLT IATMS	**	dimensionless dimensionless
TWILT -	hrs.		NBDRP	—	dimensionless
ALBED - FLSOD -	dimensionless cal/m²/min.		TBDRP BRATE	-	min. g/min.
PTINC -	hrs.		NCLDC	140	dimensionless
DTMAX - SPHTW -	min. cal/g/°K		TCLDC ALBC	-	min. dimensionless
SPHTG -	cal/g/°K		TBBC	100	۰K
MOLA - MOLG -	dimensionless dimensionless		NVALVE TVALVE	***	dimensionless
ALFRES -	dimensionless		VALVRT NEX	•	g/sec. dimensionless
EG - ALFSO -	dimensionless dimensionless		ELN1	-	hrs.
TWSOL - RWSOL -	dimensionless dimensionless		ELN2 ELN3		min. sec.
EW -	dimensionless		TT(1)	-	hrs.
RW - TAUW -	dimensionless dimensionless		TT(2) TT(3)	-	min. sec.
TASL -	oK		EMB	_	millibars
HTROP - TATRO -	o.K		EAIRT EFILMT	-	°C
HTROP2 - TATROP2 -	m		EGAST	-	°Č

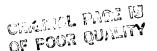


Table 3. Summary of Input Default Values

TIMOL = 18.0	TWSOL = 0.885
CUTDT = 24.0	RWSOL = 0.114
BALT = 120.0	EW = 0.031
ASCRT = 304.8	RW = 0.127
HFLIT = 36700.0	TAUW = 0.842
PASL = 1013.3	TASL = 288.15
MASSF = 1.842E5	HTROP = 11000.0
MGAS = 6.9221E4	TATROP = 215.65
MPAYI = 1.9682E5	HTROP2 = 20000.0
VOLMAX = 6.6375E4	TATR02 = 216.65
DAYL = 12.0	HTROP3 = 32000.0
TWILT = 0.75	TATR03 = 228.65
ALBED = 0.18	HFLOT = 47000.0
FLSOD = 1.9892E4	TAFLO = 270.65
PTINC = 0.01666	HBB2 = 11000.0
DTMAX = 5.0	HBB3 = 20000.0
SPHTW = 0.55	T2T = 214.4
SPHTG = 1.24119	T3T = 214.4
MOLA = 28.9644	T4T = 214.4
MOLG = 4.0026	DPLT = -1.0
ALFRES = 0.0026	IATMS = 5
EG = 0.000312	RGAS = 8.31432E7
ALFSO = 0.001	EDOTG = 0.0

Table 4. List of FORTRAN variable names used within the program

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	Description
-	Surface area of balloon (m ²)
-	Acceleration due to gravity (m/min ²)
-	Effective infrared absorptance of balloon gas
	Array of Albedo factors corresponding to times TCLDC(I)
-	Current Albedo factor (0.18 for clear skies; 0.57 maximum)
-	Absorptance of balloon gas
-	Absorptance of balloon film
-	Estimated balloon ascent rate (m/min)
-	Subroutine to compute balloon altitude in meters when
	the altitude is given in millibars of pressure
-	Effective infrared absorptance of balloon film
-	Plotting subroutine (plots axes)(Local)
-	Launch altitude (m)
-	Array of ballast rates corresponding to times TBDRP(I)(g/min.)
-	Thermal conductivity of air (calorie/min/m/°K)
-	Coefficient of drag
-	Function subprogram to compute the heat transfer coefficient
	between the balloon film and air
	Thermal conductivity of helium
	Heat transfer coefficient between balloon film and air

FORTRAN Variable	Description ORIGINAL PAGE IS OF POOR QUALITY
CHF	- Forced convection coefficient between balloon film and air
CHN	- Natural convection coefficient between the balloon film and air
CHR	- Heat transfer coefficient between the balloon film and gas
CHRES	- Function subprogram to compute the heat transfer coefficient
	between the balloon film and gas
CIT	- Parameter used to determine relationship of the sun to the
	balloon (day/night)
CUTDT	- Length of flight to be simulated (hrs.)
DAYL	- Length of daylight (hrs.input; converted to min. within program)
DINCH	- Time of day (hrs.)
DPLT	- Positive value of DPLT generates plotted output
DTIME	- Time increment (min.)
DTIMEN	- Minimum time increment (min.)
DTMAX	- Maximum time increment (min.)
DTMIN	- Plotting time scale increment (min./inch of plot)
DX 1	- Plotting time scale increment (min./inch of plot)
EAIRT(I)	- Array of measured ambient air temperature (°C) corresponding
	to the array of times ETIME(I)
EALT(I)	- Array of measured altitudes (m) corresponding to the array
	of times ETIME(I)
EDOTG	- Gas volume flow rate for "burping" of gas when float altitude
	is exceeded (m ³ /sec)
EDOTV(I)	- Array of gas mass flow rate during valving operation (g/sec.)
	corresponding to the array of time TVALVE(I)

EG - Emissivity of the balloon gas

EGAST(I) - Array of measured balloon gas temperature (°C) corresponding to the array of times ETIME(I)

EGEF - Effective emissivity of the balloon gas

EINT - Effective interchange emissivity between the balloon gas and film

ELANCH - Launch time (sec.) = 3600.*ELNI+60.*ELN2+ELN3

ELN1 - See ELANCH (hrs.)

ELN2 - See ELANCH (min.)

ELN3 - See ELANCH (sec.)

EMB1(I) - Array of In (pressure at launch site/EMB(I)); plotting parameter

ETIME(I) - Array of times for which measured temperature and altitude

data have been input (sec) = 3600.*TT(1)+60.*TT(2)+T(3)
ELAUNCH

EW - Emissivity of the balloon film

EWEF - Effective emissivity of the balloon film

EXPO - Exponent used in computing the pressure, density and temperature as a function of balloon altitude

EXPT - Exponent used in computing the pressure, density and temperature as a function of balloon altitude

EXP2 - Exponent used in computing the pressure, density and temperature as a function of balloon altitude EXP3 - Exponent used in computing the pressure, density and temperature as a function of balloon altitude

FK1, FK2, FK3, FK4, FL1, FL2, FL3, FL4, FM1, FM2, FM3, FM4, FN1, FN2, FN3, FN4, F01, F02,

F03,F04 ~ Runge Kutta parameters of the general form:

$$y_i(t+dt)=y_i(t)+1/6$$
 (Fi1+2Fi2+2Fi3+Fi4)
for i = K,L,M,N,O

FLIFT - Free lift on the balloon (kg)

FLSOD - Solar radiation constant (1.9892 10⁴ cal/m²/min)

FLXSD - Solar radiation flux adjusted for the time of day

FMTOT - Total mass of balloon system minus the mass of gas (kg)

F1

- Right hand sides of the five governing first order ordinary differential equations.

F4

F5

F2

F3

GR - Grashof Number

GY - Acceleration due to gravity (m/sec²) in Subroutine ATMOS2

H - Parameter in subroutine ATMOS2 to designate altitude (m)

- HB Parameter in subroutine ATMOS2 to designate the base altitude of the various layers of the standard atmosphere (m)
- HBAL Altitude of balloon (m)
- HBB2 Black ball altitude corresponding to black ball temperature T2T in a black ball temperature-altitude three segment profile (m)
- in a black ball temperature-altitude three segment profile (m)
- HFLIT Estimated float altitude (m) used to determine TIMFL. When time exceeds TIMFL, TBBC(I) used instead of three segment TBB profile.
- HFLOT Nominal float altitude (m)
- HMGAS Duplicate storage location for the mass of gas during each time increment (g)
- HTR Duplicate storage location for the balloon gas temperature during each time increment (°K)
- HTROP Altitude corresponding to the atmosphere temperature TATRO in a four segment temperature-altitude profile (m)
- HTROP2 Altitude corresponding to the atmosphere temperature TATRO2 in a four segment temperature-altitude profile (m)
- HTROP3 Altitude corresponding to the atmosphere temperature TATRO3 in a four segment temperature-altitude profile (m)
- HTS Duplicate storage location for the balloon film temperature during each time increment (°K)
- HVOLG Duplicate storage location for the balloon volume during each time increment (m^3)

FORTRAN Variable		Description
HZ1	-	Balloon altitude during each time increment (m)
HZ2	-	Balloon velocity during each time increment (m/sec)
IATMS	-	Parameter to choose atmospheric model, i.e.,
		IATMS = 1 NSBF Winter Atmosphere
		2 NSBF Spring Atmosphere
		3 NSBF Summer Atmosphere
		4 NSBF Fall Atmosphere
		5 1962 Standard Atmosphere
		6 User supplied atmosphere
IPC	-	Printer control character
ITC		Parameter used in varying the time 'ncrement of the
		solution of the governing differential equations
IVOL	-	Parameter used to identify regions of the flight that
		"burping" of balloon gas is required
IVT	•••	Parameter used to adjust the volume flow rate of the
		gas during the "burping" process
KUTTA	-	Parameter used to direct the Runge-Kutta solution of
		the governing ordinary differential equations
LINE	-	Local system subroutine used in the plot portion of the program
LP	-	Lapse rate of the layers of the 1962 standard atmosphere
		as contained in subroutine ATMOS2
MA	-	Molecular weight of air (Subroutine ATMOS2 parameter)
MASSF	-	Mass of balloon film (g)

MGAS - Mass of gas(g) MGASD - Increment of the mass of gas for each time step of the solution MOLA - Molecular weight of air (main program) MOLG - Molecular weight of balloon gas MPAY - Mass of the balloon payload (g) MPAYI - Mass of the balloon payload at launch including ballast (g) MPD(I) - Array of mass of balloon payload associated with time of ballast drops TBDRP(I) NBDRP - (Number of ballast drops + 1) * 2; input number of ballast	FORTR Variab		Description ORIGINAL PAGE IS OF POOR QUALITY
MGASD - Increment of the mass of gas for each time step of the solution MOLA - Molecular weight of air (main program) MOLG - Molecular weight of balloon gas MPAY - Mass of the balloon payload (g) MPAYI - Mass of the balloon payload at launch including ballast (g) MPD(I) - Array of mass of balloon payload associated with time of ballast drops TBDRP(I)	MCAC		Mana of gan(.)
solution MOLA - Molecular weight of air (main program) MOLG - Molecular weight of balloon gas MPAY - Mass of the balloon payload (g) MPAYI - Mass of the balloon payload at launch including ballast (g) MPD(I) - Array of mass of balloon payload associated with time of ballast drops TBDRP(I)			•••
 MOLG - Molecular weight of balloon gas MPAY - Mass of the balloon payload (g) MPAYI - Mass of the balloon payload at launch including ballast (g) MPD(I) - Array of mass of balloon payload associated with time of ballast drops TBDRP(I) 	כאטויו	<i>u</i> -	
 MPAY - Mass of the balloon payload (g) MPAYI - Mass of the balloon payload at launch including ballast (g) MPD(I) - Array of mass of balloon payload associated with time of ballast drops TBDRP(I) 	MOLA		Molecular weight of air (main program)
 MPAYI - Mass of the balloon payload at launch including ballast (g) MPD(I) - Array of mass of balloon payload associated with time of ballast drops TBDRP(I) 	MOLG	-	Molecular weight of balloon gas
<pre>MPD(I) - Array of mass of balloon payload associated with time of ballast drops TBDRP(I)</pre>	MPAY	-	Mass of the balloon payload (g)
ballast drops TBDRP(I)	MPAY	I -	Mass of the balloon payload at launch including ballast (g)
	MPD(I) -	· •
drops required	NBDR	Р	(Number of ballast drops + 1) * 2; input number of ballast drops required
NCLDC - (Number of cloud cover and/or black ball regions in the flight simulation) + 1; input number of cloud cover or black ball	NCLD	C -	simulation) + 1; input number of cloud cover or black ball
regions required for the simulation			•
NEX - Number of measured data points input		-	·
NEX1 - NEX + 1			
NEX2 NEX + 2			
NPC - Printer control character			
NPSUN - Parameter to eliminate the influence of the sun during the	NPSU	N -	Parameter to eliminate the influence of the sun during the
night portion of the flight simulation			night portion of the flight simulation
NSUN - Parameter to eliminate the influence of the sun during the	NSUN	-	Parameter to eliminate the influence of the sun during the
night portion of the flight simulation			night portion of the flight simulation
NTITLE(I) - Array for storage of an 80 character title	NTIT	LE(I) -	Array for storage of an 80 character title
NVALVE - (Number of gas valvings during the flight +1) * 2; input number of valvings required for the flight simulation	NVAL	VE -	
NYC - Number of data points collected for plotting	NYC	-	· · · · · · · · · · · · · · · · · · ·
NYCP1 - NYC + 1		1 -	· · · · · · · · · · · · · · · · · · ·
NYCP2 - NYC + 2			
PA - Atmospheric pressure in subroutine ATMOS2 (millibars)		_	

FORTRAN Variable

Description

PASL - Ambient air pressure at the launch site (mb)

PATRO - Ambient air pressure at HTROP (mb)

PATRO2 - Ambient air pressure at HTROP2 (mb)

PATRO3 - Ambient air pressure at HTROP3 (mb)

PB - Balloon gas pressure (mb)

PB1(I) - Array of pressure altitude parameters corresponding to the array of times XPTT(I). PB1 = ln (PASL/PB)

PLOT - System subroutine used in plotting phase of program

PLOTS - System subroutine used in plotting phase of program

PR - Prandtl Number

PTIMH - Time of day in hours (Data are printed and saved for

PTINC - Time increment in hours | plotting in time increments of PTINC

OF - Rate of heat transfer to the balloon film

QG - Rate of heat transfer to the balloon gas

R - Radius of balloon (Main program and subprograms CFH and CHRES)

- Universal gas constant (subprogram ATMOS2)

REY - Reynold's number

RGAS - Universal gas constant

RHOB - Air density at the base of the layers of the 1962 Standard

Altitude in subprogram ATMOS2

RRES - Diameter of the balloon (subprogram CHRES)

RW - Infrared reflectivity of the balloon film

RWSOL - Ultraviolet reflectivity of the balloon film

SIGMA - Stefan-Boltzmann constant

SPHTG - Specific heat of the balloon gas

FORTRAN Variable

Description

SPHTW - Specific heat of the balloon film

STOR - Temporary storage location for the balloon gas viscosity

TA - Ambient air temperature (°K)

TAFLO - Air temperature corresponding to altitude HFLOT in the four segment air temperature profile (°K)

TAK - Ambient air temperature (°C)

TASL - Air temperature at launch (°K)

TATRO - Air temperature corresponding to altitude HTROP in a four segment air temperature profile (°K)

TATRO2 - Air temperature corresponding to altitude HTROP2 in a four segment air temperature profile (°K)

TATRO3 Air temperature corresponding to altitude HTROP3 in a four segment air temperature profile (°K)

TAUW - Infrared transmittance of the balloon film

TB - Air temperature at the base of the atmospheric layer of the 1962 Standard Atmosphere in subprogram ATMOS2

TBB - Black ball temperature (°K)

TBBC(I) - Array of black ball temperatures corresponding to the cloud cover array ALBC(I) and the array of times TCLDC(I). Used when time exceeds TIMFL. $({}^{O}K)$

TBDRP(I) - Array of times associated with the ballast drops of the simulated flight (min.)

TIME - Time of day at each point of the flight simulation (min)

FORTRAN Variable		Description
TIMFL	-	Estimated time to float. Computed from ASCRT and HFLIT.
TIMH	-	Time of day at each point of the flight simulation (hrs)
TIMH1	-	Time from launch at each point of the flight simulation (min)
TIMIO	-	Temporary storage of time of launch (min)
TIMM		Time from launch of each point of the flight simulation
		(min)
TIMOL	-	Time of launch (hrs. local standard time input; converted to minutes within program)
TIMSR	-	The Committee (1)
TIMSS	-	Time of sunset (min)
TOHIGH	-	A parameter in subroutine ATMOS2 which indicates when the
		atmospheric pressure input is less than the capability
		of the subroutine and thus corresponds to an altitude
		that is too high to be accurately modeled by the sub-
		routine
TR	-	Temperature of the balloon gas (°K)
TRDEL	-	Increment of the gas temperature during each step of the
		Runge-Kutta solution of the governing ordinary dif-
		ferential equations (°K)
TRK		Temperature of the balloon gas (°C)
TS	-	Temperature of the balloon film (°K)
TSDEL		Increment of the film temperature during each step of the

ential equations (°K)

Runge-Kutta solution of the governing ordinary differ-

FORTRAN Description Variable TSK Temperature of the balloon film (°C) Maximum allowable change in balloon film temperature during TSL each solution step See ETIME(I) TT(I) Time from sunset or sunrise (min.) TTIME Plotting parameter. Minimum temperature to be plotted (°C) TTMIN TTS - Time associated with starting conditions (min.) TVALVE(I) - An array of times corresponding to changes in valving rates (min) TWILT Length of twilight (hrs) TWSCL - Ultraviolet transmittance of the balloon film T1 - Temperature of the air in subprogram CFH (°K) T1T Black ball temperature corresponding to altitude BALT in the black ball temperature profile (°K) T2T - Black ball temperature corresponding to altitude HBBZ in the black ball temperature profile (°K) T3T - Black ball temperature corresponding to altitude HBB3 in the black ball temperature profile (°K) T4T - Black ball temperature corresponding to altitude HFLOTin the black ball temperature profile (°K). Used for altitudes above HFLOT UMU - Viscosity of the balloon gas or ambient air, as appropriate

VALVRT(I) - Array of valving mass flow rates corresponding to the times

TVALVE(I) (g/sec)

FORTRAN Variable

Description

VOLG - Volume of the balloon (m³)

VOLMAX - Maximum volume of the balloon (m³)

Thermediate value in the computation of both the heat transfer coefficient between the film and gas (subprogram CHRES) and the heat transfer coefficient between the film and air (subprogram CFH)

XLT - Physical length of the time axis on all plots (in)

XLT1 - Physical spacing between sets of axes in the plotting (in)

XLT2 - Physical spacing between sets of axes in the plotting (in)

XPTT(I) - Array of times corresponding to the arrays of computed values of gas temperature, YPT3; air temperature, YPT1; film temperature, YPT2; balloon altitude, YPH; and the pressure altitude parameter, PB1 (min)

YPT1(I) - Array of air temperatures, corresponding to the array of times XPTT(I), to be plotted (°C)

ZSL - Maximum allowable change in balloon altitude during each time step of the solution (m)

Z1 - Balloon altitude (m)

FORTRAN Variable		Description
Z1 DEL	ü	Increment of balloon altitude during each time step of the solution (m)
Z 2	1439	Balloon vertical velocity (m/min)
zadel	***	Increment of balloon vertical velocity during each time
		step of the solution (m/min)

Table 5. Summary of Program Output

Printed Output

- 1.) Heading
- 2.) Listing of input data in namelist FIPUT
- 3.) Tabular listing of the input ballast drop schedule:
 <u>Time of ballast drop (sec) Ballast rate (g/min)</u>
 (NBDRP values printed)
- 4.) Tabular listing of the input cloud cover details:

 <u>Time of cloud cover</u> (sec) <u>Albedo</u> <u>Blackball Temp. (OK)</u>

 (NCLDC values printed)
- 5.) Tabular listing of the input valving schedule:
 <u>Time of the valving (sec) Valve rate (g/min)</u>
 (NVALVE values printed)
- 6.) Tabular listing of the input measured data from the balloon flight being simulated: <u>Time(sec.) Altitude(m) Air Temp.(°C) Film Temp.(°C) Gas Temp.(°C)</u> (NEX values printed)
- 7.) The computed values of the effective emissivity of the balloon gas, the effective emissivity of the balloon film, and the effective interchange emissivity between the balloon gas and film.
- 8.) The computed values of the effective infrared absorptance of the balloon gas and the effective infrared absorptance of the balloon film.

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- 9.) Tabular listing of the computed results:

 Time(min), Altitude(m), Velocity(m/min), Air Temp. (OC),

 Film Temp. (OC), Balloon volume(m), Solar Flux, Blackball

 Temp. (OK), Free lift (kg), Pressure altitude (millibars),

 Mass of gas (g), Reynold's number, Coefficient of Drag,

 Payload mass (g)
- 10.) The total number of data points saved for plotting (NYC).

Plotted Output (Requires local subroutines equivalent to AXIS1, PLOT, PLOTS, LINE)

- A plot of the computed balloon altitude-time history and a plot of the measured balloon altitude-time history (if NEX is not 0), on a single set of axes.
- 2.) Plots of the computed balloon film and gas temperature and the ambient air temperature as functions of flight time. Also plots of measured values of film, gas and air temperature if NEX is not 0.

Reference

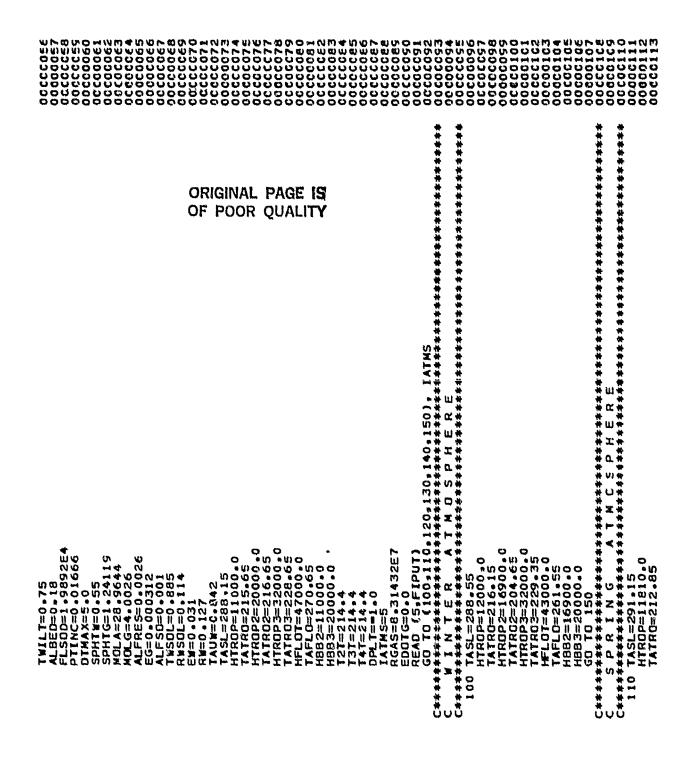
1. Carlson, L.A. and Horn, W.J., "A Unified Thermal and Vertical Trajectory Model for the Prediction of High Altitude Balloon Performance," Texas Engineering Experiment Station Report TAMRF-4217-81-02, June, 1981.

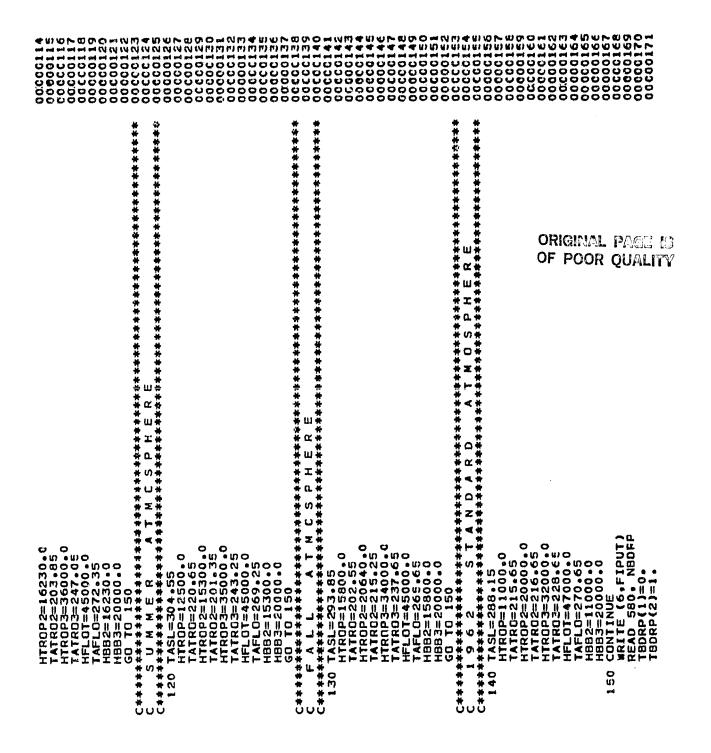
APPENDIX A PROGRAM LISTING

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                                                                                                                                                                                                                                    REAL MGAS, MOLA, WCLG, MASSF, WPAY, MPD(100), BRATE(100).

REAL MGAS, MOLA, WCLG, MASSF, WPAY, MPD(100), BRATE(100).

TEDRP(100), TCLDC(10), ALBC(10), TPBC(1C), TVALVE(25), VALVRT(25), NAMELIST /C'IPUT/ TIMOL, CUTDT, BALT, ASCRT, FFLIT, PASL, MASSF, MGAS, MPAYI, VOLMAX, CAYL, TWILT, ALBED, FLSCD, PTINC, DIMAX, SPHTW, SPHTG, MOLA, MOLA
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HFL IT=36700.0
PASL=1013.3
MASSF=1.842E5
MGAS=6.9221E4
MPAYI=1.9682E5
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TIMOL=18.0
CUTDT=24.0
BALT=120.0
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                                             0
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       56
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                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   ITC=0
TSL=1
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       READ
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READ 750, (TT(J),J=1,3),EMB(I),EAIRT(I),EFILMT(I),EGAST(I)
ETIME(I)=TT(I)*3600,+TT(2)*60,+TT(3)*ELANCH
CALL ATMGS2 (EMB(I),EALT(I),TGHIGH)
CONTINUE
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   ETIME(J), EALT(J), EAIRT(J), EFILMT(J), EGAST(J)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 150 CONTINUE
200 CGNTINUE
200 CGNTINUE
200 CGNTINUE
200 CGNTINUE
1F (NVALVE.EG.0) GC TC 220
PRINT 620
DO 210 1=1.NVALVE
READ 600, TVALVE(I).VALVRT(I)
PRINT 600, TVALVE(I).VALVRT(I)
PRINT 600, TVALVE(I).VALVRT(I)

210 CGNTINUE
220 CGNTINUE

                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               ORIGINAL PAGE IS
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                                                                                                                                                                                                                                                                                                                                                                                | DO 170 1=1,NBCFP | DO 170 1=1 | NBCFP | DO 170 1=1 | NCLDC | DO 180 | DO 180 1=1 | NCLDC | 
TBDRP(3)=2.

DO 160 I=1.3

TCLDC(I)=TEDFP(I)

BRATE(I)=0.0

TVALVE(I)=10.0

ALEC(I)=ALEED

TBEC(I)=214.4

IF (ALBED.GI.0.3) TEEC(I)=194.4

IF (NBDRP.EQ.0) &C TC 180

PRINT 590

DO 170 I=1.NBGFP
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                CONTINUE
IF (NEX.EQ.O) GC TO 260
READ 750, ELN1,ELN2,ELN3
ELANCH=3600.*ELN1+60.*ELN2+ELN3
DO 240 I=1,NEX
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       17C
180
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        240
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--ALFRES))
S)/(I.-RWSOL*(I.-ALFRES)))
                                                                 290 I=1, NVALVE
TVALVE(I)=TVALVE(I)+TIMCL
C=2.90544E=01
ROSL=1.2248
SIGMA=8.1346049E=07
AG=3.5303886E+04
TIMCL=TIMCL+60.0
TIMID=TIMCL
DO 270 I=1.NBCRP
TBDRP(I)=TINCL
                                      CONTINUE
DO 280 I=1,NCLDC
TCLDC(I)=TCLDC(I)+TIMOL
CONTINUE
                                                                                                                                                                                                                                                       TITHTASE S
DTIME=DTIMEN
NSUN=0
TTS=TIMIO
                                                          00
                                       270
                                                     280
                                                                                       300
                                                                    290
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38

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VISCOSITY GF AIR
UNU=(1.829639C1E=05=HBAL*5.06809747E=10+FBAL*FBAL*1.82009519E=14=
HBAL**3.0*1.72287567E=19)*60.0
                                                                           (TIMIO.GT.TIMCL) TTS=TIMOL
(TIS.GE.TIMSR.AND.TTS.LE.TIMSS) NSJN≔I
                                                           HTS=TS
HTR=TR
HZ1=Z2
HZ2=Z2
HMGAS=MGAS
HV0LG=V0LG
                                                                                                                           IVT=1
CONTINUE
                                                          CONTINUE
                                                                                                                                  KUTTA=1
                                                                                                                               IVOL-C
                                                                                                                             340
                          0
                                                                                                                                    69
                                                          330
                          33
                                                                                                                                    m
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360 CDITIONE

500 TILL

500 TILL

510 CDITIONE

511 E (TIME & CE - TVALVE(I)) EDCTV=VALVRT(I)

F (TIME & CE - TVALVE(I)) EDCTV=VALVRT(I)

T (TIME & CE - TVALVE(I)) EDCTV=VALVRT(I)

T (TIME & CE - TVALVE(I)) EDCTV=VALVRT(I)

T (TIME & CE - TVALVE(I))

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T (TIME & CE - TVALVE &
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         350
              400
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*FEAL , Z2, TAK, TSK, TRK, VOLG, FLXSC, TBB, FLIFT, PB, MGAS,
                                                                                                                                                                                                                                                                                                                                      12:19.1

460 CONTINUE

[F (HBAL.GE.HBB2) TBB=T1TF(HBAL-HBB2)*(TAT=T21)/(HBB2-BALT)

[F (HBAL.GT.HBB2) TBB=T2TF(HBAL-HBB2)*(TAT=T21)/(HFLGT-HBB2)

[F (HBAL.GT.HBB2) TBB=T2TF(HBAL-HBB2)*(TAT=T21)/(HFLGT-HBB3)

[F (HBAL.GT.HBB2) TBB=T2TF(HBAL-HBB2)*(TAT=T21)/(HBB2-HB2)

[F (HBAL.GT.HBB2) TBB-T2TF(HBAL-HBB2)*(TAT=T21)/(HBB2-HB2)

[F (HBAL.GT.HBB2) TBB-T2TF(HBAL-HBB2)*(TAT=T21)/(HBB2-HBAL-HBB2)

[F (HBAL.GT.HBB2) TBB-T2TF(HBAL-HBB2)*(TAT=T21)/(HBB2-HBAL-HBB2)

[F (HBAL.GT.HBB2) TBB-T2TF(HBAL-HBB2)*(TAT=TBB-TATE)

[F (HBAL.GT.HBB2) TBB-T2TF(HBAL-HBB2)*(TAT=TBB-TATE)

[F (HBAL.GT.HBB2) TBB-T2TF(HBAL-HBB2)*(TAT=TBB-TATE)

[F (HBAL.GT.HBB2) TBB-T2TF(HBAL-HBB2)*(TAT=TBB-TATE)

[F (HBAL-GT.HBB2) TBB-T2TF(HBAL-HBB2)*(TAT=TBB-TATE)

[F (HBAL-TBB-TATE)

[F (HBAL-TBB-T
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           C SECTION THE BELLAN CCMPUTATIONS
CHARACHER COMPUTATIONS
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ALBED=ALBC(I)
TO 480
T4T=TBBC(I)
                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     500
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IF (IIC.LI.2) GC TO SIO
IF (IIC.LI.2) GC TO SIO
DIIME=2.0*DTIME
ITC.0
10 CONTINUE
IF (DIIME.GE.CIFAX) CTIWE=DTWAX
NPSUN=NSUN
IF (IIME.GE.CIFAX) CTIWE=DTWAX
NPSUN=NSUN
IF (IIME.GE.CIFAX) CTIWE=DTWAX
NPSUN=NSUN
IF (IIME.GE.CIFAX) CTIWE=DTWAX
NSUN=NSUN
IF (IIME.GE.CIFAX) CTIWE=TIWES) NSUN=1
IF (NSUN.EQ.N) TIWE=CII-LIMSS
IF (NSUN.EQ.N) TIWE=CII-TIMSS
                                                                                                                                                                                                                                                      COLL PLOTS (0.0.0)

TIMIN==120.0

DIMIN==120.0

DIMIN==120.0

DIMIN==120.0

DIMIN==120.0

DIMIN==120.0

DIMIN==120.0

DIMIN==120.0

DIMIN==120.0

DIMIN==120.0

EXTT(NYCP1)=0.0

TIMIN=EX+1

NEX==NEX+1

EALT(NEX2)==DTMIN

EALT(NEX2)==DTMIN

EALT(NEX2)==DTMIN

EALT(NEX2)==DTMIN

EALT(NEX2)==DTMIN

EMBI(NEX1)==TMIN

EMBI(NEX1)==TMIN

EMBI(NEX1)==1.0

CONTINUE

XLI=XPTI(NYC)/XPTI(NYCP2)

XLI=XPTI(NYC)/XPTI(NYCP2)

YPH(NYCP1)=0.0

YPH(NYCP1)=0.0
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CALL AXISI (0.0,C.0,TIME=WIN,"=8,XLT.00.C,C.0,DX1,20.0)
CALL LINE (XFTT.PUPL=WIN,"=8,XLT.00.C,C.0,DX1,20.0)
CALL LINE (XFTT.PUPL-WIN,"10.9.0,90..C.,YPH(NYCP2),20.)
FF(NEX_LE.0)GC TC $43
CALL LINE
CALL LINE
CALL LINE
TYTI(NYCP1)=TTHIN
YPT3(NYCP1)=TTHIN
YPT3(NYCP1)=TTHIN
YPT3(NYCP1)=TTHIN
YPT3(NYCP1)=TTHIN
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570 FORMAT (1M1,20A4)
560 FORMAT (10; 1 TEDRP BALLAST RATE(GM/MIN);)
600 FCRMAT (3F10,2)
610 FORMAT (30; 1 TCLDC ALEEDC BLACKBALL(DEG=K);)
610 FORMAT (10; 1 TYALVE VALVE RATE (GM/MIN);)
620 FORMAT (10; 2 TYALVE VALVE RATE (GM/MIN);)
630 FORMAT (10; 3 TYALVE VALVE RATE (GM/MIN);)
630 FORMAT (10; 3 TYALVE VALVE RATE (GM/MIN);)
640 FORMAT (10; 3 TYALVE VALVE RATE (GM/MIN);)
650 FORMAT (10; 3 TYALVE VALVE RATE (GM/MIN); 3 TAKC); 3 TAKC);
650 FORMAT (1M1, 3 TIME; 2 TY, 4 TYALVE (M/MIN); 3 TAKC); 3 TAKC);
650 FORMAT (1M1, 3 TIME; 3 TY, 4 TAKC); 3 T
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IF (PA.LT.54.745) GPB=22E.32
HB=11000.
TB=216.65
LP=0.0
RHOB=0.36392
GO TO 70
IF (PA.LT.8.680) GC
HB=20000.
TB=216.088035
GO TO 70
IF (PA.LT.1.105) GC
HB=32000.
TB=228.65
LP=0.0028
RHOB=0.013225
GO TO 70
IF (PA.LT.0.550) GC
HB=370.065
LP=0.0028
RHOB=0.014276
GO TO 70
IF (PA.LT.0.550) GC
HB=270.65
LP=0.0014276
GO TO 70
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RHOB=0.0014276
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                       REAL MA.LP
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R=8.31432E03
GY=9.80665
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FB=0.0
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TOHIGH==1 GD TO 90 7C IF (LP.EQ.0.0) GC TO 80 H=HB+TB/LP*((PE/PA)**(LP*R/GY/MA)=1.0) GO TC 90 30 H=ALOG(PB/PA)*R*TB/GY/HA+HB 30 H=ALOG(PB/PA)*R*TB/GY/HA+HB

APPENDIX B

SAMPLE CASE

The input and output for a sample case is presented on the following pages. The 167N flight launched from Palestine, Texas on July 24, 1980, was chosen because it involves most of the features of the THERMTRAJ program with the exception of programmed valving. The plotted output should provide a good indication of the accuracy of the program in terms of predicted altitude as well as balloon gas and film temperature.

Table 1.B. TKERMTRAJ input data for the 167N flight (* Designates the column numbers of the data cards)

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	18.20.49. 19.32.49. 19.42.49.	7.03 5.04	-30.9 -29.5	-36.4 -34.0	-42.1 -36.4 -25.9	=44.5 =37.7 =27.7	⊶43.7 -40.4 -25.5
	19.50.49. 19.04.48. 19.10.49.	4.85 4.78	=28.8 =29.5 =26.5	=31.7 =30.4 =31.5	-20.0 -19.5	=21 · 4 =20 · 8	-16.8 -16.8
	19.20.49.	4.91	=26.2 =27.0	=31 .2 =31 . 2	-17.9 -18.6	-19.2 -19.6	-16.1 -17.4
	19.44.49.	4.97 5.13	=27.0 =24.5	-31 · 2 -31 · 3	=16.8 =16.2	≠19.6 =18.1 =17.4	-16.1 -14.6 -15.3
	27.28.49. 27.29.45. 27.45.28.	5.58 5.85	-24.9 -26.5 -28.3	∞31.5 ≈33.0 ∞34.8	-19.0 -18.2	=19.0 =18.1	710.7 m1%.6
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	24.30.47.	7.28 7.70	=35.6 =34.8	=37.7 =29.2	=20.2 =20.6	=22.1 =22.3 =21.6	<pre>=16.6 =17.0 =16.3</pre>
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	25.30.47 25.45.59 26.01.27	9.60	-35.3 -36.7	-41.2 -44.6	=23.0 =29.1	-21.8 -25.2	→18·1 -27·2
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	27.30.23. 27.47.51. 28.03.51	29.3	=50.4 =49.4	-49.9 -50.8	-46.0 -48.8	=42.4 =49.2	-45.2 -45.2
	28.15.51	26.1 26.1	=49.7 =49.7	-51.5 -52.6 -52.3	=49.2 =49.7 =49.9	=45.8 =50.4 =50.7	=49.2 =50.1 =50.4
	28.46.46 29.26.47 29.18.47	26.3	=53.2 =49.1 =48.2	-51.6 -51.0	-49.8 -49.1	-50 • A -50 • I	≈50.0 ≈49.3
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	30.03.57	69.8	-48.3 -49.4 -46.8	-51.7 -52.0 -51.6	=48.1 =49.7 =49.1	#50.5 #50.₫	=50.3 =49.8
	30.44.56 31.00.56 31.20.58	. 29.2	=49.8 =51.8	-51.6 -52.8	-48.7 -50.1	=49.6 =51.3	-49.5 -50.5
	31.32.58	. 29.3 . 29.8	-51.6 -52.0	-53.3 -53.5	∞50.2 ≈50.1	#51.3 #51.3 #51.3	=50.7 =50.9 =50.8
	32.16.56	. 70.3	-51.2 -51.1 -52.3	-53.3 -53.2 -55.4	-49.8 -49.4 -51.3	=50.7 =52.8	-50.7 -52.3
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Table 2.B. THERMTRAJ printed output for the 167N flight

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REY NO 0.24E+04 0.15E+04 0.74E+01 0.58E+03	0.33E+04 0.98E+04 0.15E+05 0.18E+05	0.25E+05 0.29E+05 0.32E+05 0.35E+05 0.39E+05	0.41E+05 0.45E+05 0.48E+05 0.51E+05 0.54E+05	0.57E+05 0.60E+05 0.53E+05 0.66E+05 0.66E+05	0.656m+0 0.656m+0 0.656m+0 0.65m+0 0.69m+0 0.69m+0	0.72E+05 0.74E+05 0.77E+05 0.80E+05	0.85E+05 0.88E+05 0.91E+05 0.94E+05	0.10E+06 0.10E+06 0.10E+06 0.10E+06	0.10E+06 0.10E+06 0.10E+06 0.10E+06
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VCLUME(M3) C.46499E+05 O.465C8E+05 O.46538E+05 G.465405 O.46531E+05	0.46501E+05 0.46457E+05 0.46329E+05 0.46086E+05 C.45599E+05	0.45198E+05 0.44730E+05 0.44204E+05 0.43633E+05 C.43014E+05	0.42200E+05 0.41501E+05 0.40769E+05 0.40010E+05	0.38429E+05 0.37614E+05 0.36787E+05 0.35952E+05	0.34354E+05 0.32694E+05 0.32899E+05 0.32194E+05	C.30797E+05 0.20101E+05 0.29405E+05 0.28712E+05	0.27335E+05 0.25654E+05 0.25979E+05 0.25312E+05	0.24005E+05 0.23380E+05 0.22786E+05 0.22203E+05	0.211206+05 0.206116+05 0.201236+05 0.196546+05
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PAY(GE) 196820. 196820. 196820. 196820.	10000000000000000000000000000000000000	196820• 196820• 196820• 196820•	196820. 196820. 196820.	196820. 196820. 196820.	195820. 192534. 185730. 177792.	174140- 174140- 174140- 174140-	174140. 174140. 174140. 174140.	174140. 174140. 174140. 174140.	174140. 174140. 174140. 174140.
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767 NO 0.85E+05 0.84E+05 0.84E+05 0.84E+05	0.63E+05 0.83E+05 0.82E+05 0.82E+05	0.81E+055 0.81E+055 0.81E+055 0.80E+05	0.80E+0S 0.79E+0S 0.79E+0S 0.79E+0S	0.79E+05 0.79E+05 0.79E+05 0.78E+05	0.78E+05 0.16E+05 0.30E+06 0.36E+06	0.23E+06 0.15E+06 0.95E+05 0.49E+05	0.29E+05 0.30E+05 0.28E+05 0.25E+05 0.25E+05	0.11E +05 0.24E +05 0.25E +05 0.19E +05	0.22E+05 0.22E+05 0.16E+05 0.21E+05 0.23E+05
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VCLUME(M3) 0.84788E+04 0.63838E+04 C.82998E+04 C.81999E+04	0.80239E+04 0.79389E+04 C.78556E+09 0.77739E+04 C.76941E+04	0.76558E+04 0.75392E+04 0.74641E+04 C.73904E+04	C.72475E+04 C.71780E+04 C.71058E+04 0.70428E+04	0.69123E+04 C.68487E+04 C.67861E+04 O.67245E+04 C.66639E+04	C.66042E+04 0.65347E+04 0.65634E+04 C.66908E+04 C.686C8E+04	C.65988E+U4 O.71524E+O4 O.72373E+O4 C.73210E+O4	C.74164E+04 O.74449E+04 O.7472IE+04 O.75235E+04	0.75834E+04 0.75991E+04 C.76144E+04 0.76409E+04 C.76693E+04	C.76916E+04 C.77109E+04 C.77845E+04 C.77842E+04
16(C) 147.04 147.15 147.46 147.46	147.74 147.87 148.00 148.14	44444 44444 6662 4662 4756 4756 6074	9444 9444 9449 9449 9449 9449 9449	4444 2444 2444 2444 2444 2444 2444 244	1111 55650 56650 56600 56000 5	######################################	1111 5555 5555 5555 5555 5555 5555 555	1111 5555 5566 5666 5666 5666 5666 5666	1111 156 156 175 175 175 175 175 175 175 175 175 175
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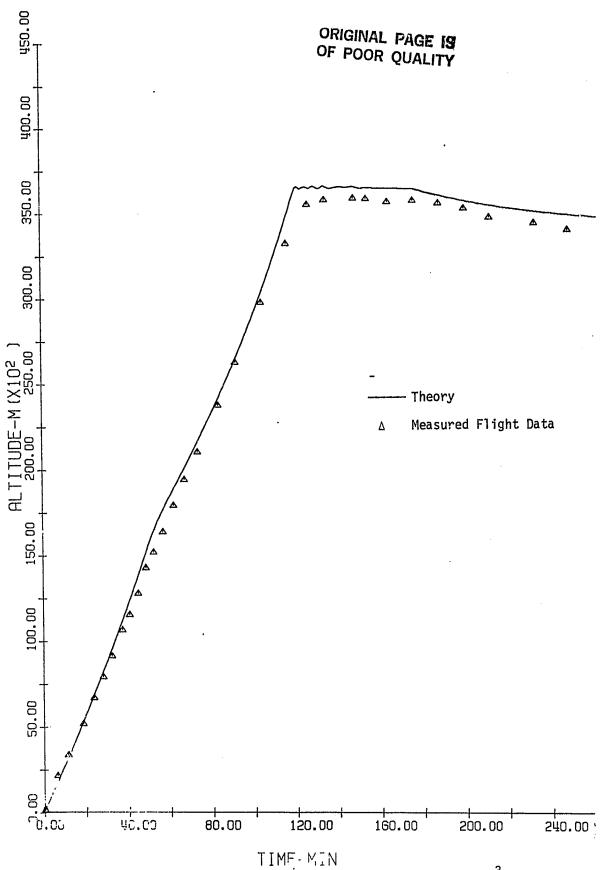


Figure 1.B. Altitude Trajectory for Flight 167N (66375 m³ balloon launched 1135 CDT, 24 July, 1980) 69

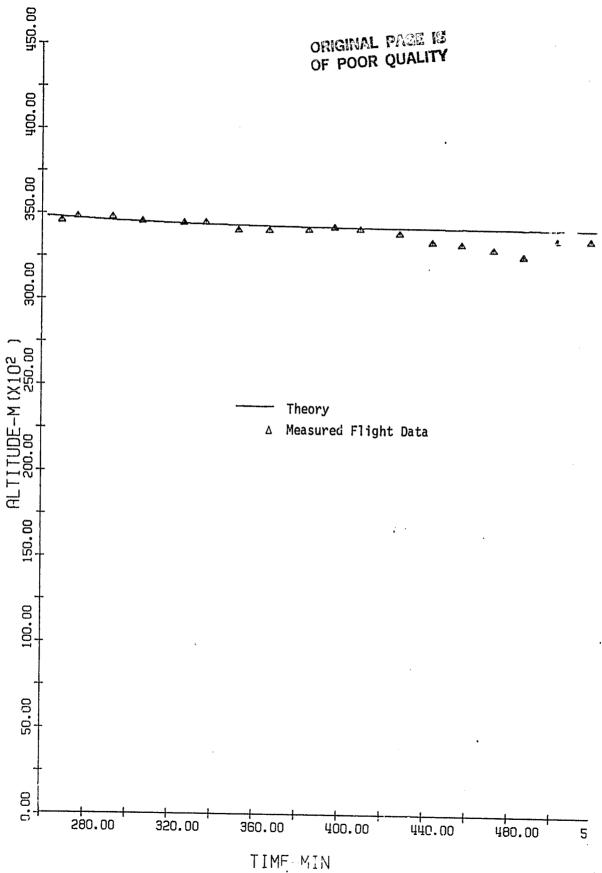


Figure 1.B. (continued) Altitude Trajectory for Flight 167N (66375 m³ balloon launched 1135 CDT, 24 July, 1980) 70

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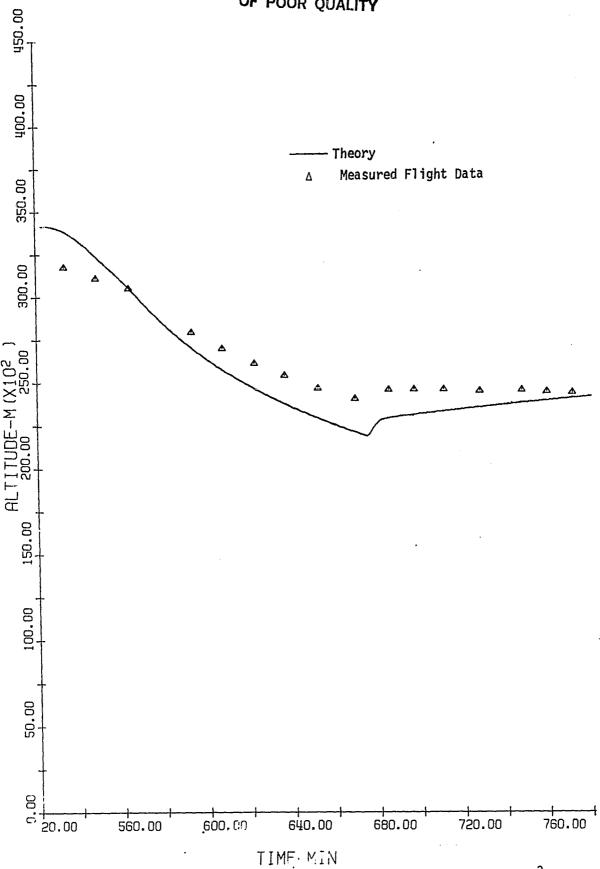


Figure 1.B. (continued) Altitude Trajectory for Flight 167N (66375 m³ balloon launched 1135 CDT, 24 July 1980) 71

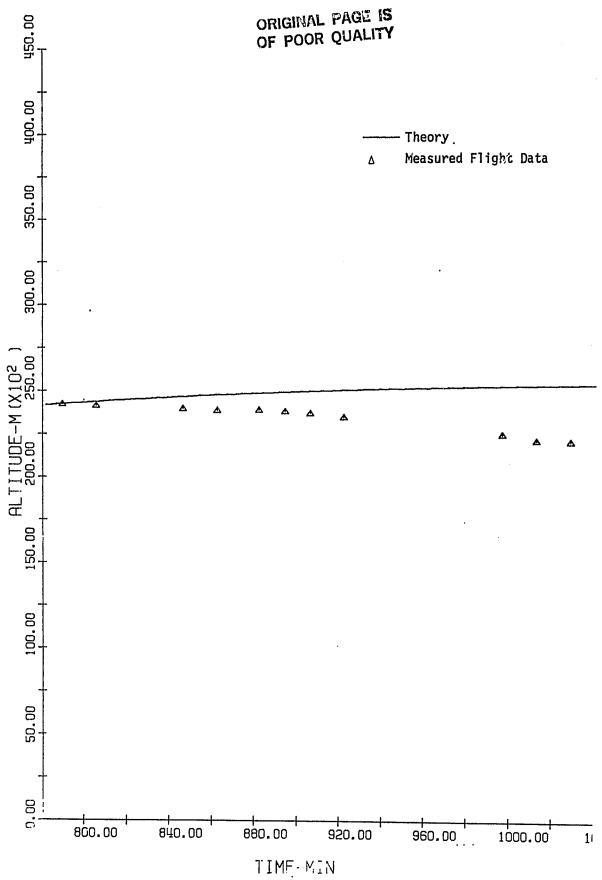


Figure 1.B. (continued) Altitude Trajectory for Flight 167N(66375 m³ balloon launched 1135 CDT, 24 July, 1980) 72

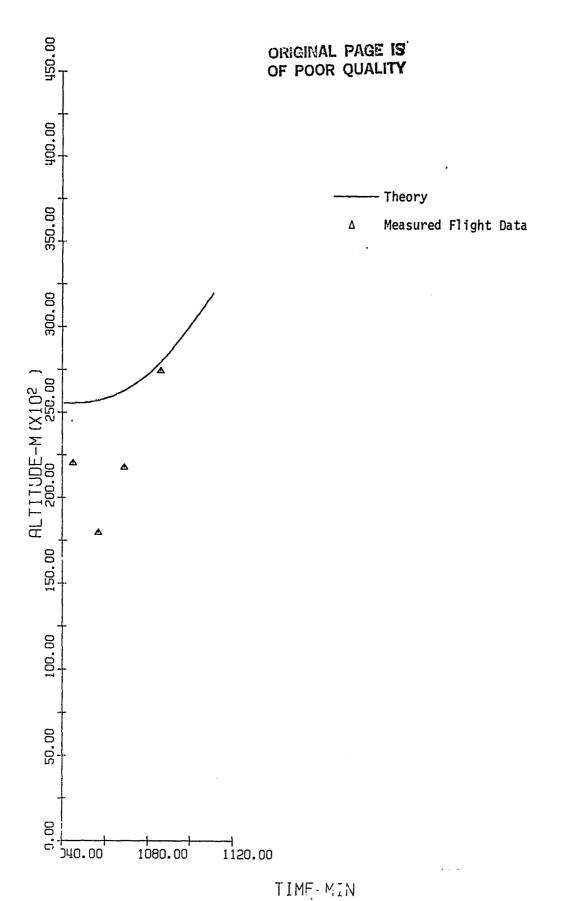


Figure 1.B. (continued) Altitude Trajectory for Flight 167N (66375 m³ balloon Taunched 1135 CDT, 24 July, 1980) 73

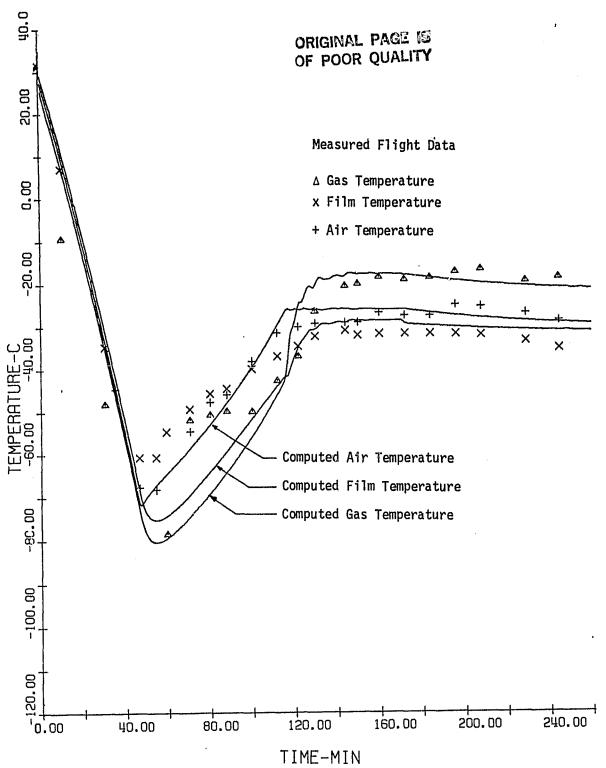


Figure 2.B. Temperature Profile for Flight 167N (66375 m³ balloon launched 1135 CDT, 24 July, 1980)

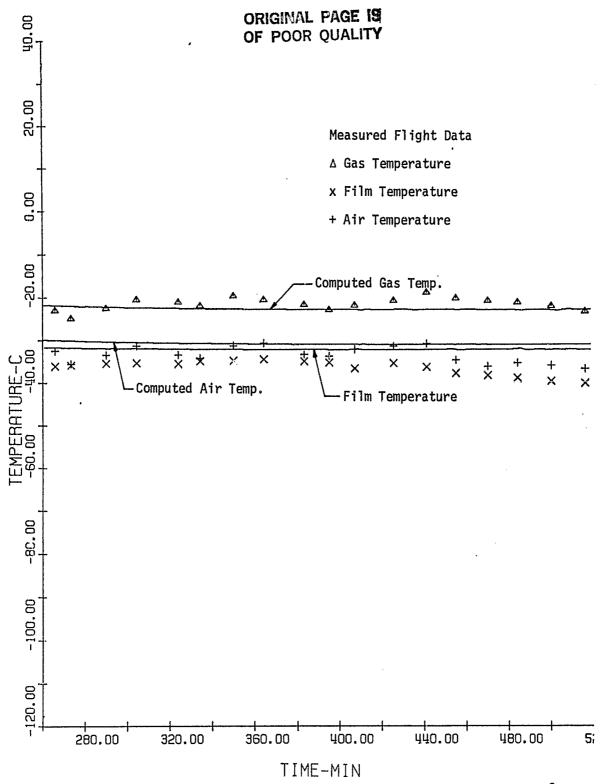


Figure 2.B. (continued) Temperature Profile for Flight: 167N(66375 m³ balloon launched 1135 CDT, 24 July, 1980)

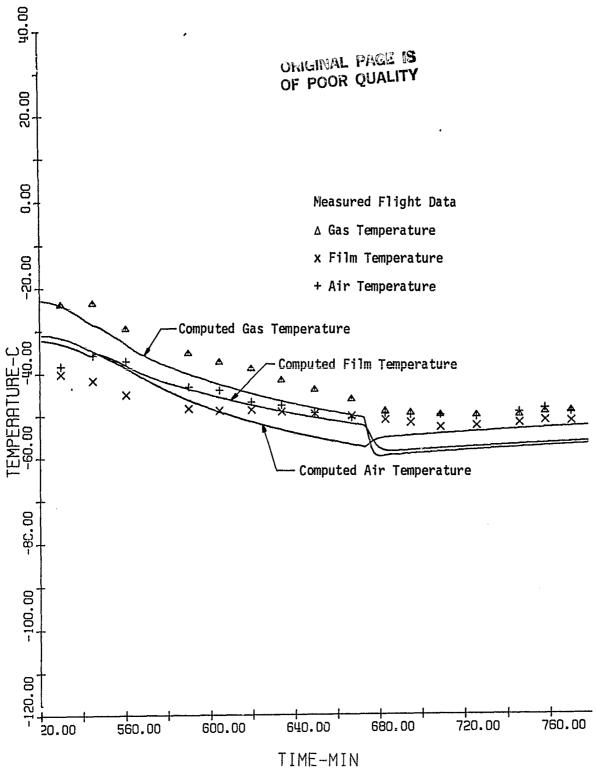


Figure 2.B. (continued) Temperature Profile for Flight 167N (66375 m balloon launched 1135 CDT, 24 July, 1980)

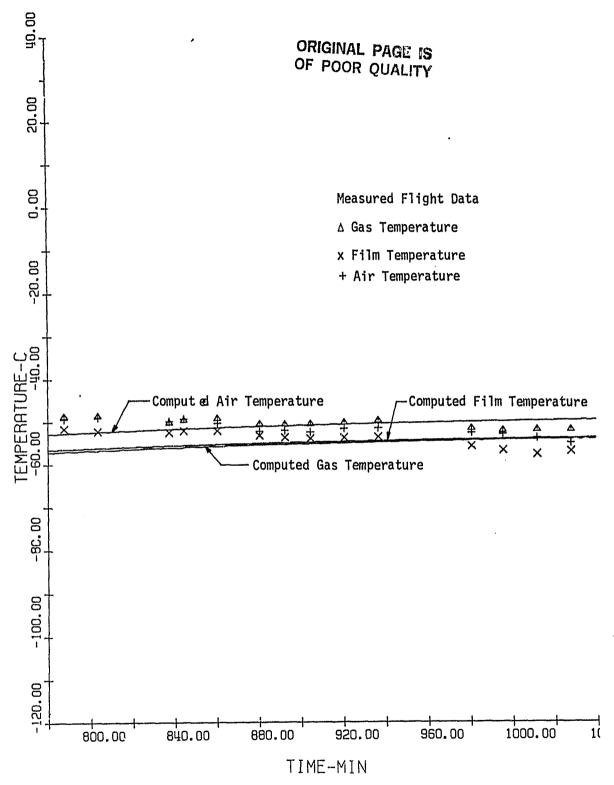


Figure 2.B. (continued) Temperature Profile for Flight 167N (66375 m³ balloon launched 1135 CDT, 24 July, 1980

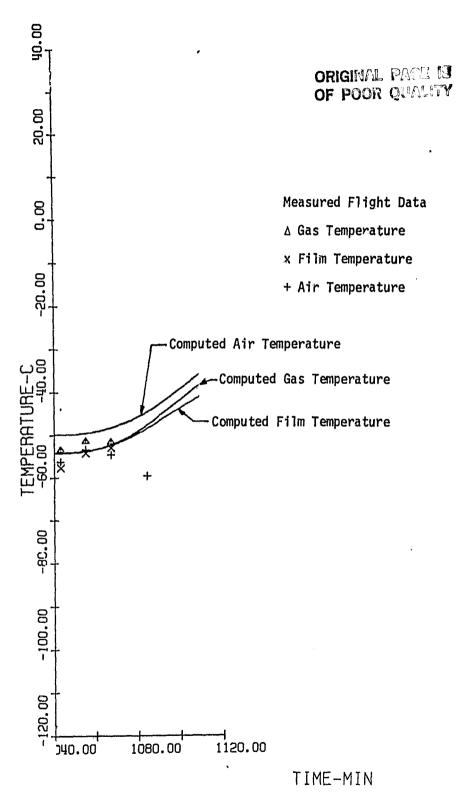


Figure 2.B. (continued) Temperature Profile for Flight
167N (66375 m³ balloon launched 1135 CDT, 24 July 1980)

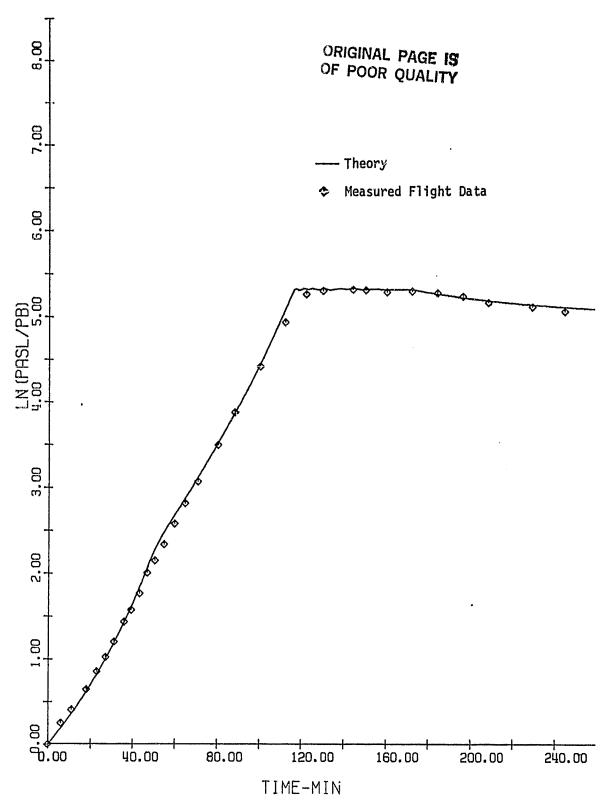


Figure 3.B. Pressure Trajectory for Flight 167N(66375 m³ balloon launched 1135 CDT, 24 July, 1980)

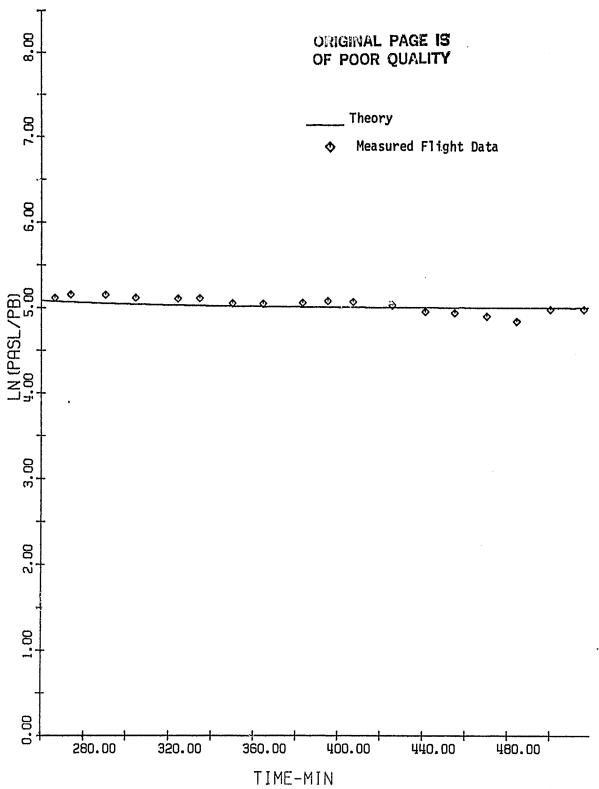


Figure 3.B. (continued) Pressure Trajectory for Flight 167N (66375 m³ balloon launched 1135 CDT, 24 July, 1980)

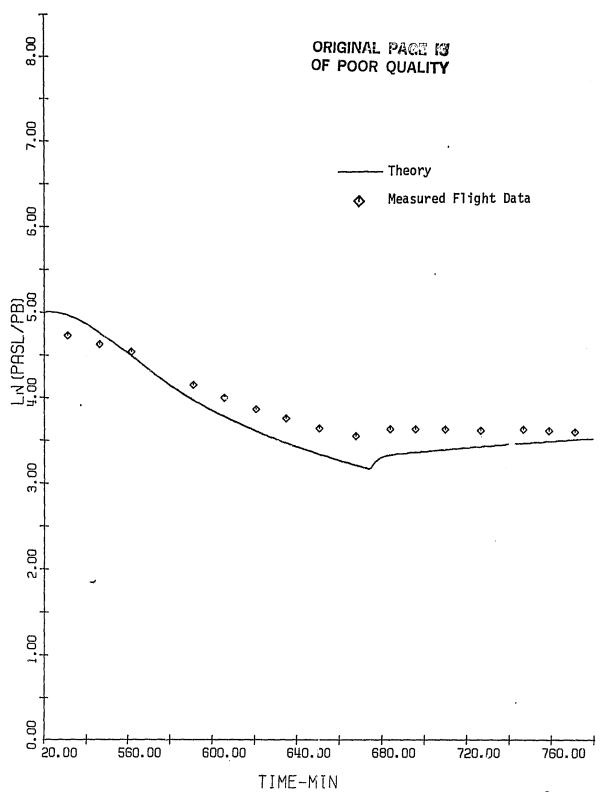


Figure 3.B. (continued) Pressure Trajectory for Flight 167N(66375 m³ balloon launched 1135 CDT, 24 July, 1980)

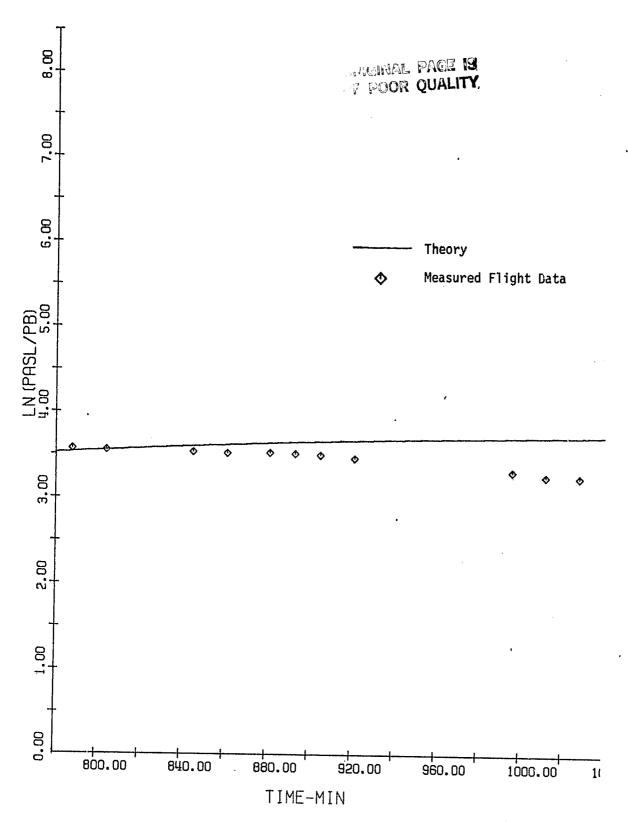


Figure 3.B. (continued) Pressure Trajectory for Flight $167N(66375 \text{ m}^3 \text{ balloon launched } 1135 \text{ CDT}, 24 \text{ July}, 1980)$

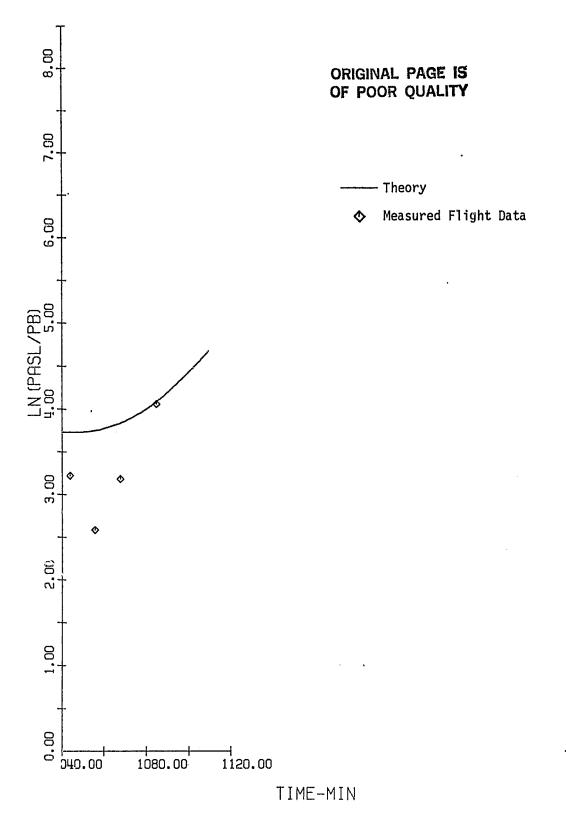


Figure 3.B. (continued) Pressure Trajectory for Flight 167N(66375 m³ balloon launched 1135 CDT, 24 July, 1980)